Reverse electrodialysis systems comprising wafer and applications thereof

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**Title:** REVERSE ELECTRODIALYSIS SYSTEMS COMPRISING WAVER AND APPLICATIONS THEREOF

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**Notice:** Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 287 days.

**Abstract:**
In one aspect, reverse electrodialysis systems are described herein having constructions operable to reduce membrane stack resistance, thereby requiring significantly less membrane surface area for meaningful electrical power generation. A reverse electrodialysis system described herein comprises an anode and cathode adjacent to a membrane stack, the membrane stack comprising alternating anion and cation exchange membranes defining diluate and concentrate ionic solution compartments, wherein an ion exchange medium is positioned in a diluate compartment.

**Claims:**
20 Claims
References Cited

U.S. PATENT DOCUMENTS

                     429/417

FOREIGN PATENT DOCUMENTS

WO  WO2008108533  *  9/2008

* cited by examiner
FIGURE 1

Anode

Cathode

CEM

AEM

- Cl⁻, Na⁺, Cl⁻, Na⁺, Cl⁻, Na⁺

- Rinse

- Storage Battery or Electrical Grid

- High Salinity Water

- Low Salinity Water

- Wafer
Effect of Ion Exchange Wafer on RED Stack Resistance

- Wafer Enhanced RED
- Traditional RED

Stack Resistance (kΩ)
Salt Concentration (g/L)

FIGURE 2
REVERSE ELECTRODIALYSIS SYSTEMS
COMPRISING WAVER AND APPLICATIONS
THEREOF

RELATED APPLICATION DATA

The present application is a U.S. National Phase of
International Application No. PCT/US2014/041343, filed
Jun. 6, 2014, which hereby claims priority pursuant to 35
No. 61/832,388 filed Jun. 7, 2013, each of which is incor-
porated herein by reference in its entirety.

FIELD

The present invention relates to reverse electrodialysis systems
and, in particular, to reverse electrodialysis systems
employing ion exchange media independent of the ion
exchange membranes.

BACKGROUND

With the increasing controversy surrounding fossil fuel
based emissions, significant resources are being devoted to
developing alternative and renewable energies. Energy pro-
duction from salinity gradients has been known for several
decades and offers significant advantages of carbonless
emissions and renewability. Two leading methods of energy
production from salinity gradients are pressure retarded
osmosis (PRO) and reverse electrodialysis (RED). Reverse
electrodialysis functions on the basis of salinity differences
in mixing solution such as sea water and river water. A
membrane stack is sandwiched by electrodes and composed of
alternating salt water and freshwater compartments
defined by anion and cation exchange membranes permitting
selective exchange of ions between the compartments.
Driven by the difference in chemical potential between the
salt water and freshwater solutions, cations diffuse through
the cation exchange membranes toward the cathode and
anions diffuse through the anion exchange membranes
toward the anode. At the electrodes, a redox couple is used
to initiate the transfer of electrons. Therefore, when elec-
trodes are connected to an external circuit, electrical power
can be extracted from the reverse electrodialysis system.

The theoretical power density of reverse electrodialysis
systems is in the neighborhood of 20 W/m². In actual
implementation, however, the power density drops signifi-
cantly to 1-3 W/m² in the most efficient systems. The
precipitous drop in power density can be attributed to
several factors including resistances through the cation and
anion exchange membranes, electrode resistance and power
consumed in plant operation. In order to compensate for
these losses, significant membrane area is required. This can
be prohibitive given the high cost and limited lifetimes of
suitable cation and anion exchange membranes.

SUMMARY

In one aspect, reverse electrodialysis systems are
described herein having constructions operable to reduce
membrane stack resistance, thereby requiring significantly
less membrane surface area for meaningful electrical power
generation. A reverse electrodialysis system described
herein comprises an anode and cathode adjacent to a mem-
brane stack, the membrane stack comprising alternating
anion and cation exchange membranes defining dilute and
concentrate ionic solution compartments, wherein an ion
exchange medium is positioned within a dilute compartment. In
some embodiments, the anion and cation exchange mem-

branes define a plurality of dilute compartments and con-

centrate compartments, wherein the ion exchange medium is
positioned within the dilute compartments.

In another aspect, methods of making reverse electrodial-
ysis systems are described herein. A method of making a
reverse electrodialysis system comprises providing a mem-
brane stack comprising alternating anion and cation
exchange membranes defining dilute and concentrate ionic
solution compartments. An ion exchange medium is posi-
tioned in the dilute compartment and an anode and cathode
are positioned adjacent to the membrane stack. In some
embodiments, the anion and cation exchange membranes
define a plurality of dilute compartments and concentrate
compartments wherein the ion exchange medium is posi-
tioned in the dilute compartments.

In another aspect, methods of generating electrical current
are described herein. A method of generating electrical
current comprises providing a reverse electrodialysis system
comprising an anode and cathode adjacent to a membrane
stack, the membrane stack comprising alternating anion and
cation exchange membranes defining dilute and concentrate
ionic solution compartments, wherein an ion exchange
medium is positioned in the dilute compartment. Dilute
ionic solution is flowed into the dilute compartment and
concentrated ionic solution flows into the concentrate
compartment. Anions from the concentrated ionic solution
are passed through the anion exchange membrane in a
direction toward the anode and cations from the concen-
trated ionic solution are passed through the cation exchange
membrane in a direction toward the cathode. An external
electrical circuit is connected to the anode and cathode to
extract electrical current from the reverse electrodialysis
system.

In some embodiments, the anion and cation exchange
membranes define a plurality of dilute compartments and con-
centrate compartments, wherein the ion exchange medium is
positioned in the dilute compartments. Dilute
ionic solution is flowed into the dilute compartments and
concentrated ionic solution flows into the concentrate
compartments. Anions from the concentrated ionic solution
are passed through the anion exchange membranes in a
direction toward the anode and cations from the concen-
trated ionic solution are passed through the cation mem-
branes in a direction toward the cathode. An external
electrical circuit is connected to the anode and cathode to
extract electrical current from the reverse electrodialysis
system.

In a further aspect, a method of reducing membrane stack
resistance in a reverse electrodialysis system is described
herein. Such a method comprises positioning an ion
exchange medium in one or more dilute compartments of
the electrodialysis system, wherein the stack resistance is
reduced by at least an order of magnitude relative to an
identical or substantially identical membrane stack not
employing the ion exchange medium. These and other embodiments are further described in the
detailed description which follows.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 illustrates a reverse electrodialysis system accord-
ing to one embodiment described herein.

FIG. 2 illustrates reduction in stack resistance of a reverse
electrodialysis system having a construction described
herein relative to a reverse electrodialysis system of prior
construction.
Embodyments described herein can be understood more readily by reference to the following detailed description and example and their previous and following descriptions. Elements, apparatus and methods described herein, however, are not limited to the specific embodyments present in the detailed description and examples. It should be recognized that these embodyments are merely illustrative of the principles of the present invention. Numerous modifications and adaptations will be readily apparent to those of skill in the art without departing from the spirit and scope of the invention.

I. Reverse Electrodialysis Systems

In one aspect, reverse electrodialysis systems are described herein having constructions operable to reduce membrane stack resistance, thereby requiring significantly less membrane surface area for meaningful electrical power generation. A reverse electrodialysis system described herein comprises an anode and cathode adjacent to a membrane stack, the membrane stack comprising alternating anion and cation exchange membranes defining diluate and concentrate ionic solution compartments, wherein an ion exchange medium is positioned in a diluate compartment. In some embodiments, the anion and cation exchange membranes define a plurality of diluate compartments and concentrate compartments, wherein the ion exchange medium is positioned within the diluate compartments.

Turning now to specific components, a reverse electrodialysis system described herein comprises an anode and cathode adjacent to a membrane stack. The anode and cathode can be constructed of any material and have any dimensions not inconsistent with the objectives of the present invention. For example, the cathode and/or anode can be formed of a material selected from the group consisting of lead, PbO₂, titanium, PbO₂ on titanium, platinum on titanium, iridium on titanium, stainless steel, iron, zinc, nickel, copper, other metals and alloys thereof.

As described herein, the membrane stack of the reverse electrodialysis system comprises alternating anion and cation exchange membranes defining diluate and concentrate ionic solution compartments. In some embodiments, the alternating anion and cation exchange membranes define a single diluate compartment and a single concentrate compartment. Moreover, the alternating anion and cation exchange membranes can define a plurality of diluate compartments and a plurality of concentrate compartments. The membrane stack can have any desired number of anion and cation exchange membranes not inconsistent with the objectives of the present invention. The number of anion and cation exchange membranes can be selected according to several considerations including the desired number of diluate and concentrate compartments in the system. For example, the number of anion and cation exchange membranes in a reverse electrodialysis system described herein can sum to a value up to 400 or 500.

Anion exchange membranes for use in reverse electrodialysis systems described herein include membranes under the FUMASEP® trade designation, such as FUMASEP® FAS and FAB. Suitable anion exchange membranes also include Tokuyama NEOSEPTA® membranes such as Tokuyama AMX, AMH and ACM. Anion exchange membranes are also commercially available from Amerside. Typical properties of anion exchange membranes employed in reverse electrodialysis systems described herein are provided in Table I.

Cation exchange membranes for use in reverse electrodialysis systems described herein also include membranes under the FUMASEP® trade designation, such as FUMASEP® FKS and FKE. Suitable cation exchange membranes can be obtained from Tokuyama such as Tokuyama CMX, CMS and CMB. Typical properties of cation exchange membranes employed in reverse electrodialysis systems described herein are provided in Table II.

| TABLE I |
|-----------------|-----------------|
| Ion Exchange Capacity | 0.6-2.0 meq/g |
| Selectivity | >90% |
| Ohmic Resistance | <10 Ω-cm |
| Thickness | 0.5-5 mm |

| TABLE II |
|-----------------|-----------------|
| Cation Exchange Membrane Properties | |
| Ion Exchange Capacity | 0.6-2.0 meq/g |
| Selectivity | >90% |
| Ohmic Resistance | <10 Ω-cm |
| Thickness | 0.5-5 mm |

The anion and cation membranes define diluate and concentrate compartments for receiving diluate ionic solution and concentrated ionic solution respectively. The diluate and concentrate compartments can have any dimensions not inconsistent with the objectives of the present invention. Compartment dimensions can be selected according to several considerations including ionic solution flow rates. Further, the terms diluate ionic solution and concentrated ionic solution herein are used relative to one another. For example, concentrated ionic solution in embodiments described herein demonstrates an ion concentration higher than the diluate ionic solution. Concentrated and diluate ionic solutions, in some embodiments, have salinity concentrations of 0.0001-30% total dissolved solids with the concentrated ionic solution salinity exceeding the diluate ionic solution salinity. In some embodiments, salinity of the concentrated ionic solution exceeds salinity of the diluate ionic solution by at least a factor of 5. Moreover, pH of the diluate and concentrated ionic solutions can be controlled within a range of 2-12 to avoid damage to the ion exchange membranes.

Dilute and concentrated ionic solutions for use in reverse electrodialysis systems described can be obtained from various sources. In some embodiments, dilute ionic solutions are sourced from bodies of fresh water such as lakes, rivers and/or streams. Similarly, concentrated ionic solutions can be sourced from saltwater bodies such as oceans and seas. For ease of system operation, the freshwater and salt water bodies can be adjacent to one another in the environment. Reverse electrodialysis systems, for example, can be located along estuaries or other areas where fresh and salt water bodies meet. Alternatively, dilute and/or concentrated ionic solutions can be obtained from manmade sources. In some embodiments, concentrated ionic solutions are sourced from water employed in hydraulic fracturing (fracking) operations for extracting natural gas and shale oil deposits from the earth. Locating reverse electrodialysis at hydraulic fracturing sites can permit use of the systems to power equipment used in the fracturing operation.

Ions of the diluted and concentrated ionic solutions can be monovalent of multivalent. Cations, for example, can
include alkali metal and/or alkaline earth metal ionic species. Anions of the ionic solutions can comprise halides as well as other counter anionic species commonly found in salt and fresh water bodies.

 Reverse electrodialysis systems described herein also comprise an ion exchange medium positioned in one or more dilute compartments of the membrane stack. In being disposed in diluate compartment(s), the ion exchange medium is a separate component independent of the anion and cation exchange membranes defining the diluate compartment(s). The ion exchange medium can have any compositional identity and form not inconsistent with the objectives of the present invention. For example, the ion exchange medium can comprise anion exchange resin, cation exchange resin or mixtures thereof. When comprising a combination of anion and cation exchange resins, the ratio of anion to cation resin in the medium can range from 0.1:99.9 to 99.9:0.1. In some embodiments, the ratio of anion resin to cation resin in the medium is 25:75 or 50:50.

 Cation exchange resin of the ion exchange medium can comprise strong or weak acid ion resin. Suitable commercially available strong acid resins include Amberlite IR-120, Amberlite IRP-69, Amberlite IR-118, DOWEX MARATHON 750H (H) and DOWEX MONOSPHHERE C-350. Suitable commercially available weak acid resins include Amberlite FPC3500, Amberlite Cobalamion, Amberlite IRC86, DOWEX MAC-3 and IMAC HP336.

 Anion exchange resin of the ion exchange medium can comprise strong or weak base ion resin. Suitable commercially available strong base resins include Amberlite IR-400, DOWEX MARATHON OA, DOWEX UPX CORE Mono MA-600, AMBERJET 4400 OH and Amberlite FPA90 CI. Suitable commercially available weak base resins include Amberlite FPA51, Amberlite IRA67, IMAC HP661, DOWEX 66 and DOWEX M4195.

 The ion exchange medium can be provided in various forms. In some embodiments, the ion exchange medium is provided as a wafer for positioning in a diluate compartment. The wafer formed of anion exchange resin, cation exchange resin or mixtures thereof can have a porosity of 30-60% or 40-50%. Further, the wafer can demonstrate a surface area of at least 400 m²/g. In some embodiments, for example, a wafer ion exchange medium has a surface area of 400-700 m²/g. Additional properties of a wafer ion exchange medium are provided in Table III.

### TABLE III

<table>
<thead>
<tr>
<th>Ion Exchange Medium Properties</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ion Exchange Capacity</td>
<td>≥2.0 meq/g</td>
</tr>
<tr>
<td>Fixed Charge Density</td>
<td>1-2.0 meq/l</td>
</tr>
<tr>
<td>Thickness</td>
<td>0.5-5 mm</td>
</tr>
</tbody>
</table>

Wafer synthesis, in some embodiments, is conducted by creating a mixture of anion exchange resin and/or cation exchange resin, polymer and sugar. The mixture is placed in a pneumatic press at elevated temperature and pressure for a time period sufficient to form the wafer. The wafer is cooled and submersed in water or other medium operable to dissolve the sugar, forming the pore structure of the ion exchange wafer. The wafer can be subsequently cut or otherwise worked to dimensions for placement in a diluate compartment. In some embodiments, the wafer is provided dimensions and/or shape substantially matching spacers used in membrane stacks, thereby permitting the wafer to replace spacers in membrane stacks.

In addition to wafer form, the ion exchange medium may be provided in bead form. Beads, for example, may be packed into a diluate compartment providing an ion exchange medium having the desired porosity and other properties.

As described herein, the ion exchange medium may be positioned in a single diluate compartment or multiple diluate compartments. In some embodiments, an ion exchange medium is positioned in each diluate compartment of the membrane stack. Positioning the ion exchange medium in a diluate compartment can significantly lower the electrical resistance of the compartment. In some embodiments, the electrical resistance of the diluate compartment is reduced by at least an order of magnitude. For example, a diluate compartment having an ion exchange medium positioned therein can have an electrical resistance of 0.1-5 kΩ at 0.0001-1% salinity. Reducing electrical resistance of diluate compartments can lower membrane stack resistance leading to enhanced power generation of a reverse electrodialysis system. A reduction in stack resistance can translate to significantly less membrane surface area required for commercial electric power generation making reverse electrodialysis systems more economically viable.

Additionally, in some embodiments, the ion exchange medium can be positioned in concentrate compartments.

Reverse electrodialysis systems described herein can be stationary or portable. In being portable, reverse electrodialysis systems can be transported to various sites for electrical production and can operate as stand-alone units.

II. Methods of Making a Reverse Electrodialysis System

In another aspect, methods of making reverse electrodialysis systems are described herein. A method of making a reverse electrodialysis system comprises providing a membrane stack comprising alternating anion and cation exchange membranes defining diluate and concentrate ionic solution compartments. An ion exchange medium is positioned in the diluate compartment and an anode and cathode are positioned adjacent to the membrane stack. In some embodiments, the anion and cation exchange membranes define a plurality of diluate compartments and concentrate compartments wherein the ion exchange medium is positioned in the diluate compartments. The anode and cathode are connected to an external electric circuit for the production of electrical current.

Reverse electrodialysis systems fabricated according to methods described herein can have any construction and properties detailed in Section I above. For example, components used to fabricate a reverse electrodialysis system including anode, cathode, anion and cation exchange membranes and an ion exchange medium can have any construction and properties recited for the same in Section I above.

III. Methods of Generating Electrical Current

In another aspect, methods of generating electrical current are described herein. A method of generating electrical current comprises providing a reverse electrodialysis system comprising an anode and cathode adjacent to a membrane stack, the membrane stack comprising alternating anion and cation exchange membranes defining diluate and concentrate ionic solution compartments, wherein an ion exchange medium is positioned in the diluate compartment. Dilute ionic solution is flowed into the diluate compartment and concentrated ionic solution is flowed into the concentrate compartment. Anions from the concentrated ionic solution are passed through the anion exchange membrane in a direction toward the anode and cations from the concentrated ionic solution are passed through the cation exchange membrane in a direction toward the cathode. An external
A reverse electrodialysis system having a construction illustrated in FIG. 1 was constructed. The cation exchange membranes were Fumasep FKS and the anion exchange membrane was Fumasep FAS. The dilute and concentrate compartments each held 10 mL, having dimensions of 12 cm x 7 cm. An ion exchange medium was positioned in the dilute compartment. The ion exchange medium was in the form of a porous wafer. The ion exchange wafer was synthesized by providing a mixture of 23 g anion exchange resin, 23 g cation exchange resin, 10 g of polyethylene and 15 g of sugar. The mixture was placed in a pneumatic press at 237° F. and 10,000 psi for a time period of 90 minutes. The formed wafer was then cooled and submerged in water to dissolve the sugar, providing porosity to the ion exchange wafer. The wafer was subsequently mechanically worked to shape and dimensions for placement in the dilute chamber.

A comparative electrodialysis system was also constructed the sole difference being that the dilute compartment did not comprise the ion exchange medium.

Stack resistances for the two reverse electrodialysis systems were determined at various salt concentrations as set forth in Tables IV and V.

### TABLE IV
Stack Resistance with Ion Exchange Medium

<table>
<thead>
<tr>
<th>Salt Conc. (g/L)</th>
<th>Resistance 1</th>
<th>Resistance 2</th>
<th>Resistance 3</th>
<th>Average</th>
<th>Std. Error</th>
</tr>
</thead>
<tbody>
<tr>
<td>30</td>
<td>0.5</td>
<td>0.6</td>
<td>0.64</td>
<td>0.58</td>
<td>0.0416</td>
</tr>
<tr>
<td>35</td>
<td>0.5</td>
<td>0.55</td>
<td>0.51</td>
<td>0.52</td>
<td>0.0153</td>
</tr>
<tr>
<td>45</td>
<td>0.56</td>
<td>0.61</td>
<td>0.58</td>
<td>0.58</td>
<td>0.0145</td>
</tr>
</tbody>
</table>

### TABLE V
Stack Resistance without Ion Exchange Medium

<table>
<thead>
<tr>
<th>Salt Conc. (g/L)</th>
<th>Resistance 1</th>
<th>Resistance 2</th>
<th>Resistance 3</th>
<th>Average</th>
<th>Std. Error</th>
</tr>
</thead>
<tbody>
<tr>
<td>30</td>
<td>23</td>
<td>13</td>
<td>17</td>
<td>17.67</td>
<td>2.91</td>
</tr>
<tr>
<td>35</td>
<td>12.8</td>
<td>15</td>
<td>13</td>
<td>13.6</td>
<td>0.702</td>
</tr>
<tr>
<td>45</td>
<td>14</td>
<td>16.7</td>
<td>16.2</td>
<td>15.63</td>
<td>0.829</td>
</tr>
</tbody>
</table>

The results of provided in Tables IV and V are further illustrated in FIG. 2. As detailed in the results, stack resistance is reduced an order of magnitude by placement of the ion exchange medium in the dilute chamber.

These substantial decreases in stack resistance demonstrated in Table IV translate to projected power densities for reverse electrodialysis systems employing ion exchange media in dilute compartments of various stack constructions as set forth in Table VI.

### TABLE VI
Projected Power Densities for Reverse Electrodialysis Systems Employing Ion Exchange Media

<table>
<thead>
<tr>
<th>$V_{appplied}$ (V)</th>
<th>$R_{cell\ per\ pair}$ (Ω)</th>
<th>Number of Cell Pairs</th>
<th>$R_{stack\ total}$ (Ω)</th>
<th>Power Density (W/m²)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>0.8</td>
<td>12</td>
<td>9.6</td>
<td>16.7</td>
</tr>
<tr>
<td>2.5</td>
<td>1.76</td>
<td>14</td>
<td>24.6</td>
<td>8.7</td>
</tr>
<tr>
<td>3</td>
<td>2.08</td>
<td>17</td>
<td>35.4</td>
<td>7.3</td>
</tr>
<tr>
<td>3.5</td>
<td>2.52</td>
<td>20</td>
<td>50.4</td>
<td>5.9</td>
</tr>
<tr>
<td>4</td>
<td>1.1</td>
<td>23</td>
<td>25.3</td>
<td>13.5</td>
</tr>
<tr>
<td>4.5</td>
<td>0.32</td>
<td>25</td>
<td>8.0</td>
<td>49.6</td>
</tr>
</tbody>
</table>

For comparative purposes, projected power densities for reverse electrodialysis systems of various stack constructions not incorporating ion exchange media in the dilute compartments are provided in Table VII. The projections of Table VII are based on the stack resistance values of Table V.
### Projected Power Densities for Reverse Electrodialysis Systems of Traditional Constructions

<table>
<thead>
<tr>
<th>$V_{applied} (V)$</th>
<th>$R_{cell,pair} (\Omega)$</th>
<th>Number of Cell Pairs</th>
<th>$R_{dilute,compartment} (\Omega)$</th>
<th>Power Density $(W/m^2)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>8.2</td>
<td>12</td>
<td>98.4</td>
<td>1.6</td>
</tr>
<tr>
<td>2.5</td>
<td>5.08</td>
<td>14</td>
<td>71.12</td>
<td>3.0</td>
</tr>
<tr>
<td>3</td>
<td>2.56</td>
<td>17</td>
<td>43.52</td>
<td>5.9</td>
</tr>
<tr>
<td>3.5</td>
<td>2.54</td>
<td>20</td>
<td>50.8</td>
<td>5.9</td>
</tr>
<tr>
<td>4</td>
<td>1.86</td>
<td>23</td>
<td>42.78</td>
<td>8.0</td>
</tr>
<tr>
<td>4.5</td>
<td>1.86</td>
<td>25</td>
<td>46.5</td>
<td>8.5</td>
</tr>
</tbody>
</table>

It is clear from Tables VI and VII that employment of an ion exchange medium in one or more dilute compartment of a reverse electrodialysis system significantly enhances power density of the system, especially at low applied voltage. Power densities were obtained by applying a voltage to the RED stack to simulate high cell pairs. The resulting current obtained from this applied voltage was then used in conjunction with the calculated resistance to determine the power output and power density.

Various embodiments of the invention have been described in fulfillment of the various objects of the invention. It should be recognized that these embodiments are merely illustrative of the principles of the present invention. Numerous modifications and adaptations thereof will be readily apparent to those skilled in the art without departing from the spirit and scope of the invention.

The invention claimed is:

1. A reverse electrodialysis system comprising:
   - an anode electrode and a cathode electrode adjacent to a membrane stack, the membrane stack comprising alternating anion and cation exchange membranes defining a dilute compartment and a concentrate ion solution compartment;
   - an ion exchange medium positioned in the dilute compartment, the ion exchange medium comprising a binding agent and a cation exchange resin, anion exchange resin, or a combination of both resins; and
   - an external applied voltage across the membrane stack, wherein the dilute compartment comprising the ion exchange medium has an electrical resistance of 0.1-5 kΩ at 0.0001-1% salinity.

2. The reverse electrodialysis system of claim 1, wherein the anion and cation exchange membranes define a plurality of dilute compartments and concentrate compartments, wherein the ion exchange medium is positioned in the dilute compartments.

3. The reverse electrodialysis system of claim 1, wherein the ion exchange medium comprises a porous wafer including the cation exchange resin, anion exchange resin or combination thereof.

4. The reverse electrodialysis system of claim 3, wherein the wafer has porosity of 30-60%.

5. The reverse electrodialysis system of claim 3, wherein the wafer has a surface area of at least 400 m²/g.

6. The reverse electrodialysis system of claim 1, wherein the anode and cathode are connected to an external electrical circuit for the production of electrical current.

7. The reverse electrodialysis system of claim 1 further comprising ion solution in the dilute and concentrate compartments.

8. The reverse electrodialysis system of claim 7, wherein the ion solution of the dilute compartment or concentrate compartment comprises multivalent ions.

9. The reverse electrodialysis system of claim 7, wherein the ion solution of the concentrate compartment is derived from water used in hydraulic fracturing operations.

10. The reverse electrodialysis system of claim 7, wherein the ion solution of the concentrate compartment is derived from a natural salt water body and the ion solution of the dilute compartment is derived from a natural fresh water body.

11. The reverse electrodialysis system of claim 1, wherein the system is portable.

12. The reverse electrodialysis system of claim 11, wherein the electrodes are operable for connection to electrical circuits having differing loads.

13. A method of generating electrical current comprising:
   - providing a reverse electrodialysis system comprising an anode and cathode adjacent to a membrane stack, the membrane stack comprising alternating anion and cation exchange membranes defining a dilute compartment and a concentrate ion solution compartment, wherein an ion exchange medium is positioned in the dilute compartment and comprises a cation exchange resin, anion exchange resin, or a combination of both resins;
   - flowing dilute ion solution into the dilute compartment and concentrated ion solution into the concentrate compartment;
   - applying an external voltage across the membrane stack; passing anions from the concentrated ion solution through the anion exchange membrane in a direction towards the anode and passing cations from the concentrated ion solution through the cation exchange membrane in a direction toward the cathode; and connecting an external electrical circuit to the anode and cathode to extract electrical current from the reverse electrodialysis system.

14. The method of claim 13, wherein the anion and cation exchange membranes define a plurality of dilute compartments and concentrate compartments, wherein the ion exchange medium is positioned in the dilute compartments.

15. The method of claim 14, wherein the dilute ion solution is flowed into the dilute compartments and concentrate ion solution is flowed into the concentrate compartments.

16. The method of claim 15, wherein anions from the concentrated ion solution are passed through the anion exchange membranes in a direction towards the anode and cations from the concentrated ion solution are passed through the cation exchange membranes in a direction towards the cathode.

17. The method of claim 13, wherein the ion exchange medium comprises cation exchange resin, anion exchange resin or combination thereof.

18. The method of claim 13, wherein the ion exchange medium comprises a porous wafer including the cation exchange resin, anion exchange resin or combination thereof.

19. A reverse electrodialysis system comprising:
   - an anode and cathode adjacent to a membrane stack, the membrane stack comprising alternating anion and cation exchange membranes defining dilute and concentrate ion solution compartments, wherein an ion exchange medium is positioned in the dilute compartment; and
   - an external applied voltage across the membrane stack.
20. The reverse electrodialysis system of claim 19, wherein the ion exchange medium comprises a porous wafer including a cation exchange resin, anion exchange resin, or combination thereof.